Tikrit university College of Engineering Mechanical Engineering Department

Lectures on Numerical Analysis

Chapter 3 Finite Difference Method

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What is a Finite Difference Equation?

A finite difference method (FDM) is is one of the available numerical methods for solving <u>differential equations</u> by approximating <u>derivatives</u> with <u>finite differences</u>. Both the spatial domain and time interval (if applicable) are <u>discretized</u>, or broken into a finite number of steps. In general real life EM problems cannot be solved by using the analytical methods, because?

- The PDE is not linear.
- The solution region is complex, 2.
- The boundary conditions are of mixed types, 3.
- The boundary conditions are time dependent, 4.

The numerical methods are based on replacing the *differential* equations by algebraic equations (finite difference equations).

For **finite difference** method, this is done by replacing the *derivatives* by *differences*. A function f that depends on x

The first derivative of f(x) at a point is equivalent to the *slope* of a line tangent to the curve at that point. C)

$$\frac{df(x)}{dx} = \lim_{\Delta x \to 0} \frac{\Delta f}{\Delta x} = \lim_{\Delta x \to 0} \frac{f(x + \Delta x) - f(x)}{\Delta x}$$

If we don't take the indicated limit, we will have the following *approximate* relation for the derivative:

$$\frac{df(x)}{dx} \approx \frac{f(x + \Delta x)) - f(x)}{\Delta x}$$
The differential $\frac{d(f)}{dx} \approx \frac{\Delta f}{h}$ the difference

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2



t(x)

Finite Difference Approximation Of The Derivative Steps of finite difference solution:

- Divide the solution region into a grid of nodes,
- Approximate the given differential equation by finite difference equivalent,
- Solve the differential equations subject to the boundary conditions and/or initial conditions.

The rate of the change of the function with respect to the variable x is accounted between the



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Three Basic Finite Difference Methods

In **finite difference** approximations of the slope, we can use values of the function in the neighborhood of the point to achieve the goal. There are 3 ways to express differentials of a function: **f(x) f(x)↑ 1. Forward difference** is the rate of change of the function values between the "current" step at x_i , and the function value at a step "forward" at x_{i+1} and equal to the slope of Approximated points: $(x_i, f(x_i))$ and line that connects slope the $(x_{i+1}, f(x_{i+1}))$: True

$$\frac{d(f)}{dx}\Big|_{x=x_{i}} = \frac{f(x_{i+1}) - f(x_{i})}{x_{i+1} - x_{i}} = \frac{f(x_{i+1}) - f(x_{i})}{h}$$
$$\frac{d(f)}{dx}\Big|_{x=x_{i}+1} = \frac{f(x_{i+2}) - f(x_{i+1})}{h}$$
$$\frac{d(f)}{dx}\Big|_{x=x_{i}+2} = \frac{f(x_{i+3}) - f(x_{i+2})}{h}$$

2. Backward difference is the rate of change of the function values between the "current" step at x_i , and the function value at a step "back" at x_{i-1} , which is the slope of the line that connects points: $((x_i, f(x_i)))$ and $(x_{i-1}, f(x_{i-1}))$:

$$\frac{d(f)}{dx}\Big|_{x=x_i} = \frac{f(x_i) - f(x_{i-1})}{x_i - x_{i-1}}$$
$$= \frac{f(x_i) - f(x_{i-1})}{h}$$
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f(x)

19.02.2025

 x_i

Backward difference

 x_{i+1}

h

h

 x_i

Forward difference

Approximated

slope

 $\overline{x_{i-1}}$

 x_{i+1}

True

slope

 $\overline{x_{i-1}}$

slope

X

f(x)

X

3. Central difference is the rate of change of function f(x) is accounted for between the step at back at $(x - \Delta x)$ and the step ahead of x, i.e. $(x + \Delta x)$, which is the slope of the line that connects points: $(x_{i-1}, f(x_{i-1}))$ and $(x_{i+1}, f(x_{i+1}))$: Central difference Approximated $\frac{d(f)}{dx}\Big|_{x=x_i} = \frac{f(x_{i+1}) - f(x_{i-1})}{x_{i+1} - x_{i-1}} = \frac{f(x_{i+1}) - f(x_{i-1})}{2h}$ slope The step size in above is "2h" which is "big" in compromising the accuracy. True h slope A more accurate "central difference scheme" is to reduce the step size in each forward and backward Xi **X**_{i-1} **X**_{i+1} X direction by half as show Tangent of f(x) $\Delta x = h$, the step size f(x) + at $x = x_i$ f(x) We will have the corresponding expressions: $=\frac{f(x_{i+\frac{1}{2}}) - f(x_{i-\frac{1}{2}})}{f(x_{i+\frac{1}{2}}) - f(x_{i-\frac{1}{2}})}$ 5

19.02.2025

The second order derivative

1. The forward difference scheme

1. The forward difference scheme
The second order derivative of the function at
$$x_i$$
 can be derived by the following procedure

$$\frac{\partial^2 f}{\partial x^2}\Big|_{x=x_i} = \frac{d}{dx} \left(\frac{d(f)}{dx}\right)\Big|_{x=x_i} = \lim_{\Delta x \to 0} \frac{\nabla f|_{x_{i+1}} - \nabla f|_{x_i}}{\Delta x} \approx \frac{\nabla f|_{x_{i+1}} - \nabla f|_{x_i}}{\Delta x} = \frac{\nabla f|_{x_{i+1}} - \nabla f|_{x_i}}{\Delta x}$$

$$= \frac{\nabla f|_{x_{i+1}} - \nabla f|_{x_i}}{h} = \frac{\nabla f|_{x_{i+1}} - \nabla f|_{x_i}}{h} = \frac{f(x_{i+2}) - 2f(x_{i+1}) + f(x_i)}{h^2}$$
2. The backward difference scheme
and the send order derivatives in the form:

$$\frac{d}{dx} \left(\frac{d(f)}{dx}\right)\Big|_{x=x_i} = \lim_{\Delta x \to 0} \frac{\nabla f|_{x_i} - \nabla f|_{x_{i-1}}}{\Delta x} \approx \frac{\nabla f|_{x_i} - \nabla f|_{x_{i-1}}}{\Delta x} = \frac{\nabla f|_{x_i} - \nabla f|_{x_{i-1}}}{h} = \frac{f(x_i) - 2f(x_{i-1}) + f(x_{i-2})}{h}$$
3. The central difference scheme

$$\frac{d}{dx} \left(\frac{d(f)}{dx}\right)\Big|_{x=x_i} = \lim_{\Delta x \to 0} \frac{\nabla f|_{x_i} - \nabla f|_{x_{i-1}}}{\Delta x} \approx \frac{\nabla f|_{x_i} - \nabla f|_{x_{i-1}}}{h} = \frac{f(x_i) - 2f(x_{i-1}) + f(x_{i-2})}{h^2}$$
3. The central difference scheme

$$\frac{d}{dx} \left(\frac{d(f)}{dx}\right)\Big|_{x=x_i} = \lim_{\Delta x \to 0} \frac{\nabla f|_{x_{i+1}} - \nabla f|_{x_{i-1}}}{\Delta x} \approx \frac{\nabla f|_{x_{i+1}} - \nabla f|_{x_{i-1}}}{\Delta x} = \frac{\nabla f|_{x_i} + \frac{1}{2} - \nabla f|_{x_i}}{h^2}$$

$$\frac{\partial^2 f|_{x=x_i}} = \frac{d}{dx} \left(\frac{d(f)}{dx}\right)\Big|_{x=x_i} = \lim_{\Delta x \to 0} \frac{\int f|_{x_{i+1}} - \nabla f|_{x_{i-1}}}{\Delta x} \approx \frac{\nabla f|_{x_{i+1}} - \nabla f|_{x_{i-1}}}{\Delta x} = \frac{\nabla f|_{x_i} + \frac{1}{2} - \nabla f|_{x_i}}{h^2}$$

$$\frac{\partial^2 f|_{x=x_i}} = \frac{d}{dx} \left(\frac{d(f)}{dx}\right)\Big|_{x=x_i} = \lim_{x \to 0} \frac{\int f|_{x_{i+1}} - f(x_i) - f(x_i) - f(x_i) - f(x_i)}{h} = \frac{f(x_i) - 2f(x_i) + f(x_{i-1})}{h^2}$$

$$\frac{\partial^2 f|_{x=x_i}} = \frac{d}{dx} \left(\frac{d(f)}{dx}\right)\Big|_{x=x_i} = \frac{\int f|_{x_{i+1}} - f(x_i) - f(x_i) - f(x_i) - f(x_i)}{h} = \frac{f(x_{i+1}) - 2f(x_i) + f(x_{i-1})}{h^2}$$

$$\frac{\partial^2 f|_{x=x_i}} = \frac{d}{dx} \left(\frac{d(f)}{dx}\right)\Big|_{x=x_i} = \frac{\int f|_{x_{i+1}} - f(x_i) - f(x_i) - f(x_i) - f(x_i)}{h} = \frac{f(x_{i+1}) - 2f(x_i) + f(x_{i-1})}{h^2}$$

Example : Comparing numerical and analytical differentiation.

Consider the function $f(x) = x^3$. Calculate its first derivative at point x = 3 numerically with the forward, backward, and central finite difference formulas and using:

(a) Points x = 2, x = 3, and x = 4. (b) Points x = 2.75, x = 3, and x = 3.25.

Compare the results with the exact (analytical) derivative. **SOLUTION**

Analytical differentiation: The derivative of the function is $f'(x) = 3 x^2$ and the value of the derivative at x = 3 is $f'(3) = 3 (3^2) = 27$.

The points used for numerical differentiation are:

x	2	3	4 •	f(x)	N
f(x)	8	27	64		→ ∧v

Using the derivatives the forward, backward, and central finite difference formulas are: Forward finite difference

$$\frac{d(f)}{dx}\Big|_{x=x_i} = \frac{f(x_{i+1}) - f(x_i)}{h} \bigoplus \frac{d(f)}{dx}\Big|_{x=3} = \frac{f(4) - f(3)}{4 - 3} = \frac{64 - 27}{1} = 37 \quad error = \left|\frac{37 - 27}{27} \times 100\right| = 37.04\%$$

Backward finite difference

$$\frac{d(f)}{dx}\Big|_{x=x_i} = \frac{f(x_i) - f(x_{i-1})}{h} \Rightarrow \frac{d(f)}{dx}\Big|_{x=3} = \frac{f(3) - f(2)}{3 - 2} = \frac{27 - 8}{1} = 19 \quad error = \left|\frac{19 - 27}{27} \times 100\right| = 29.63\%$$

Central finite difference

$$\frac{d(f)}{dx}\Big|_{x=x_i} = \frac{f(x_{i+1}) - f(x_{i-1})}{2h} \oint \frac{d(f)}{dx}\Big|_{x=3} = \frac{f(4) - f(2)}{4 - 2} = \frac{64 - 8}{2} = 28 \quad error = \left|\frac{28 - 27}{27} \times 100\right| = 3.704\%$$
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(b)The points used for numerical differentiation are:

x	2.75	3	3.25
f(x)	2.75 ³	27	3.25 ³

Nazza Using the derivatives the forward, backward, and central finite difference formulas are: sur Forward finite difference

Finite Difference Schemes of partial derivatives

For a function f(x,y) with two independent variables, the partial derivatives with respect to x and y at the point (x_i, y_i) can be approximated into three basic scheme :

1. Forward difference is the rate of change of the function values between the "current" step at (x_i, y_j) , and the function value at a step "forward" at (x_{i+1}, y_j)):

$$\frac{\partial f}{\partial x}\Big|_{\substack{x=x_i \\ y=y_j}} = \frac{f(x_{i+1}, y_j) - f(x_i, y_j)}{x_{i+1} - x_i} = \frac{f(x_{i+1}, y_j) - f(x_i, y_j)}{h_x}$$
$$= \frac{f(x_{i+1}, y_j) - f(x_i, y_j)}{h_x}$$
$$= \frac{f(x_i, y_{j+1}) - f(x_i, y_j)}{h_y}$$

 $\begin{array}{c}
\frac{\partial f}{\partial y} \\
f(x,y) \\
f(x_1,y) \\
(x_2,y) \\
(x_3,y) \\
(x_5,y) \\
x
\end{array}$

v 🔺

2. Backward difference is the rate of change of the function values between the "current" step at x_i , y_{j_i} , and the function value at a step "back" at x_{i-1} , y_j , :

$$\frac{\frac{\partial f}{\partial x}}{\begin{vmatrix} x = x_i \\ y = j \end{vmatrix}} \frac{f(x_i, y_j) - f(x_{i-1}, y_j)}{x_i - x_j - 1} = \frac{f(x_i, y_j) - f(x_{i-1}, y_j)}{h_x}$$
$$= \frac{f(x_i, y_j) - f(x_{i-1}, y_j)}{h_x}$$
$$\frac{\frac{\partial f}{\partial y}}{y = y_j} \frac{x = x_i}{y = y_j} = \frac{f(x_i, y_j) - f(x_i, y_{j-1})}{y - y_{j-1}} = \frac{f(x_i, y_j) - f(x_i, y_{j-1})}{h_y}$$



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The second order derivative

The second order derivative of the function

The second order derivative of the function
at x and y can be derived by the following
$$\frac{\partial^2 f}{\partial x^2} \Big|_{\substack{x=x_i \\ y=y_j}} \frac{f(x_{i+1},y_j)-2f(x_i,y_j)+f(x_{i-1},y_j)}{h^2_x}$$

$$\frac{\partial^2 f}{\partial y^2} \Big|_{\substack{x=x_i \\ y=y_j}} \frac{f(x_i,y_{j+1})-2f(x_i,y_j)+f(x_i,y_{j-1})}{h^2_y}$$

$$y_i$$

$$y_i$$

$$x_1$$

$$x_2$$

$$x_i$$

$$x_n$$

$$\frac{\partial^2 f}{\partial x \partial y} \Big|_{\substack{x=x_i \\ y=y_j}} \frac{[f(x_{i+1},y_{j+1})-f(x_{i-1},y_{j+1})] - [f(x_{i+1},y_{j-1})-f(x_{i-1},y_{j-1})]}{2h^2_x h^2_y}$$

$$y$$

$$\frac{1}{y_i}$$

$$\frac{1}{y_i$$

Т

Example 1

The deflection y in a simply supported beam with a uniform load q and a tensile axial load T is given by $y \uparrow$

$$\frac{d^2 y}{dx^2} - \frac{Ty}{EI} = \frac{qx(L-x)}{2EI}$$

Where

X =location along the beam (in).

T = tension applied (lbs)

E = Young's modulus of elasticity of the beam (psi). B

I= second moment of area (in^4)

- Q= uniform loading intensity (lb/in)
- L= length of beam (in)

y(x=0) = 0 y(x=L) = 0

Figure 3 Simply supported beam for Example

Given, T = 7200 lb, q = 5400 lbsin, L = 75 in E = 30 Msi , and I = 120 in⁴ a) Find the deflection of the beam at x = 50'' Use a step size of $\Delta x = 25$ '' and approximate the derivatives by central divided difference approximation. **Solution**

a) Substituting the given values,

$$\frac{d^{2}y}{dx^{2}} - \frac{7200y}{(30 \times 10^{6})(120)} = \frac{(5400)x(75 - x)}{2(30 \times 10^{6})(120)}$$

$$\frac{d^{2}y}{dx^{2}} - 2 \times 10^{-6} y = 7.5 \times 10^{-7} x(75 - x)$$
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(1)
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19.02.2025

Approximating the derivative $\frac{d^2y}{dx^2}$ at node *i* by the central divided difference approximation,

 $\frac{d^2 y}{dx^2} - 2 \times 10^{-6} y = 7.5 \times 10^{-7} x(75 - x)$

Figure central difference method.

 $f(x_{i+1}) - 2f(x_i) + f(x_{i-1})$

 h^2

i+1

i = 4

x = 75

13

19.02.2025

i-1

$$\frac{d^{2} y}{dx^{2}} \approx \frac{y_{i+1} - 2y_{i} + y_{i-1}}{(\Delta x)^{2}}$$

We can rewrite the equation as

$$\frac{y_{i+1} - 2y_i + y_{i-1}}{(\Delta x)^2} - 2 \times 10^{-6} y_i = 7.5 \times 10^{-7} x_i (75 - x_i)$$

Since $\Delta x = 25$, we have 4 nodes as given in Figure 3 The location of the 4 nodes then is

$$x_{1} = 0$$

$$x_{2} = x_{1} + \Delta x = 0 + 25 = 25$$

$$x_{3} = x_{2} + \Delta x = 25 + 25 = 50$$

$$x_{4} = x_{3} + \Delta x = 50 + 25 = 75$$
Writing the equation at each node, we get to x=75 with $\Delta x = 25$.
Node 1: From the simply supported boundary condition at $x = 0$ we obtain
$$y_{1} = 0$$
Node 2: Rewriting equation (1) for node 2 gives
$$\frac{y_{3} - 2y_{2} + y_{1}}{(25)^{2}} - 2 \times 10^{-6} y_{2} = 7.5 \times 10^{-7} x_{2}(75 - x_{2})$$
0.0016 $y_{1} - 0.003202y_{2} + 0.0016y_{3} = 9.375 \times 10^{-4}$
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$$y_{1} = 0$$

$$x = 1 \quad i = 2 \quad i = 3 \quad i = 4$$

$$x = 0 \quad x = 25 \quad x = 50 \quad x = 75$$
Figure Finite difference method from $x = 0$ to $x = 75$ with $\Delta x = 25$.
$$x = 0 \quad x = 25 \quad x = 50 \quad x = 75$$

$$x = 0 \quad x = 25 \quad x = 50 \quad x = 75$$
Figure Finite difference method from $x = 0$ we obtain
$$y_{1} = 0$$
Node 2: Rewriting equation (1) for node 2 gives
$$y_{3} - 2y_{2} + y_{1} - 2 \times 10^{-6} y_{2} = 7.5 \times 10^{-7} x_{2}(75 - x_{2})$$

$$0.0016y_{1} - 0.003202y_{2} + 0.0016y_{3} = 9.375 \times 10^{-4}$$
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$$y_{1} = 0$$

$$x = 0 \quad x = 25 \quad x = 50 \quad x = 75$$

$$x = 50 \quad x = 75$$

$$x = 0 \quad x = 25 \quad x = 50 \quad x = 75$$

$$x = 0 \quad x = 0 \quad x = 0$$

$$x = 0 \quad x = 0 \quad x = 0$$

$$x = 0 \quad x = 0 \quad x = 0$$

$$y_{1} = 0$$

$$y_{2} = 2x + y_{1} - 2 \times 10^{-6} y_{2} = 7.5 \times 10^{-7} (25)(75 - 25)$$

$$y_{2} = 2x + y_{1} - 2 \times 10^{-6} y_{2} = 9.375 \times 10^{-7} (25)(75 - 25)$$

$$y_{2} = 2x + y_{1} - 2 \times 10^{-6} y_{2} = 9.375 \times 10^{-4}$$

$$y_{2} = 2x + y_{1} + y_{2} = 2x + y_{1}$$

Node 3: Rewriting equation (E1.4) for node 3 gives

$$\frac{y_4 - 2y_3 + y_2}{(25)^2} - 2 \times 10^{-6} y_3 = 7.5 \times 10^{-7} x_3 (75 - x_3)$$

$$\frac{y_{i+1} - 2y_i + y_{i-1}}{(\Delta x)^2} - 2 \times 10^{-6} y_i = 7.5 \times 10^{-7} x_i (75 - x_i)$$

$$0.0016y_2 - 0.003202y_3 + 0.0016y_4 = 7.5 \times 10^{-7} (50)(75 - 50)$$

$$0.0016y_2 - 0.003202y_3 + 0.0016y_4 = 9.375 \times 10^{-4}$$
Node 4: From the simply supported boundary condition at $x = 75$, we obtain $y_4 = 0$
 $y_1 = 0$
 $0.0016y_2 - 0.003202y_2 + 0.0016y_3 = 9.375 \times 10^{-4}$

$$0.0016y_2 - 0.003202y_3 + 0.0016y_4 = 9.375 \times 10^{-4}$$

$$0.0016y_2 - 0.003202y_3 + 0.0016y_4 = 9.375 \times 10^{-4}$$

$$0.0016y_2 - 0.003202y_3 + 0.0016y_4 = 9.375 \times 10^{-4}$$

form as

$$\begin{bmatrix} 1 & 0 & 0 & 0 \\ 0.0016 & -0.003202 & 0.0016 & 0 \\ 0 & 0.0016 & -0.003202 & 0.0016 \\ 0 & 0 & 0 & 1 \end{bmatrix} \begin{bmatrix} y_1 \\ y_2 \\ y_3 \\ y_4 \end{bmatrix} = \begin{bmatrix} 0 \\ 9.375 \times 10^{-4} \\ 9.375 \times 10^{-4} \\ 0 \end{bmatrix}$$

The above equations can be solved using on of the iterative methods such as the Gauss-Siedel method). Solving the equations we get,

$$\begin{bmatrix} y_1 \\ y_2 \\ y_3 \\ y_4 \end{bmatrix} = \begin{bmatrix} 0 \\ -0.5852 \\ -0.5852 \\ 0 \end{bmatrix} \quad y(50) = y(x_2) \approx y_2 = -0.5852$$
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19.02.2025

 $x\frac{d^2y}{dx^2} + y = 0$ **Example :-** Solve the following differential equation where 120 Subject to boundary condition y(1) = 1, y(2) = 2Solution x_{i-1} $x_{i-\frac{1}{2}}$ x_i $\frac{\partial^2 f}{\partial x^2} = \frac{f(x_{i+1}) - 2f(x_i) + f(x_{i-1})}{h^2}$ $\frac{\partial^2 f}{\partial x^2} = \frac{y_{i+1} - 2y_i + y_{i-1}}{h^2}$ $x_i = 1 + ih_i$ nh = 1, we know that $0 \leq i \leq n$, and let n = 4, by substituting into the main equation, one obtain $x_i \frac{y_{i+1} - 2y_i + y_{i-1}}{h^2} + y_i = 0 \qquad n = 4 = \frac{1}{h},$ $16 x_i y_{i+1} + (1 - 32x_i)y_i + 16 x_i y_{i-1} = 0$ (1)Substituting (i=1,2,3) into the above equation, one obtain $39 y_1 - 20 y_2 + 0 y_3 = 20$ $24 y_1 - 47 y_2 + 24 y_3 = 0$ $0 y_1 - 28 y_2 + 55 y_3 = 56$ x_1 x_2 x_3 *x*₄ =2 $x_0 = 1$ Using gauss elimination method, one obtain $y_3 = 1.85053$ $y_1 = 1.3512$, $y_2 = 1.63495$ 15 19.02.2025

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Discretization methods (Finite Difference) using Taylor Series Expansion

• Taylor's series expansion:

Consider a continuous function of x, namely, f(x), with all derivatives defined at $x + \Delta x$ Then, the value of f at a location can be estimated from a Taylor series expanded about point x, that is

$$f(x + \Delta x) = f(x) + \frac{\partial f}{\partial x} \Delta x + \frac{1}{2!} \frac{\partial^2 f}{\partial x^2} (\Delta x)^2 + \frac{1}{3!} \frac{\partial^3 f}{\partial x^3} (\Delta x)^3 + \dots + \frac{1}{n!} \frac{\partial^n f}{\partial x^n} (\Delta x)^n + \dots$$

In general, to obtain more accuracy, additional higher-order terms must be included.

• Higher order derivatives are unknown and can be dropped when the distance between grid points is small.

Taylor Series



Finite Difference Approximations of the First Derivative using the Taylor Series (forward difference)



Finite Difference Approximations of the First Derivative using the Taylor Series (backward difference)





Second Derivative Centered Difference Approximation (central difference)

$$f(x_{i+1}) = f(x_i) + f'(x_i)h + \frac{f''(x_i)}{2!}h^2 + \frac{f^{(3)}(x_i)}{3!}h^3 + \cdots$$
(1)

$$f(x_{i-1}) = f(x_i) - f'(x_i)h + \frac{f''(x_i)}{2!}h^2 - \frac{f^{(3)}(x_i)}{3!}h^3 + \cdots$$
(2)

$$f(x_{i+1}) + f(x_{i-1}) = 2f(x_i) + f''(x_i)h^2 + 2\frac{f''(x_i)}{4!}h^4 + \dots$$
(1)+(2)

$$f''(x_i) = \frac{f(x_{i+1}) - 2f(x_i) + f(x_{i-1})}{h^2} + 2\frac{f^{(4)}(x_i)}{4!} + \frac{1}{4!} + \frac{1}{4!}$$

$$f''(x_i) \approx \frac{f(x_{i+1}) - 2f(x_i) + f(x_{i-1})}{h^2} + O(h^2)$$



Higher Order Finite Difference Approximations

$$f'(x_{i}) = \frac{f(x_{i+1}) - f(x_{i})}{h} + \frac{f''(x_{i})}{2!}h + \frac{f^{(3)}(x_{i})}{3!}h^{2} + \dots + \frac{f^{(n)}(x_{i})}{n!}h^{n-1} + \dots$$

$$f''(x_{i}) = \frac{f(x_{i+2}) - 2f(x_{i+1}) + f(x_{i})}{h} - hf^{(3)}(x_{i}) + \dots$$

$$f'(x_{i}) = \frac{f(x_{i+1}) - f(x_{i})}{h} + \frac{\left[\frac{f(x_{i+2}) - 2f(x_{i+1}) + f(x_{i})}{h} + hf^{(3)}(x_{i}) + \dots\right]}{h}$$

$$+ \frac{f^{(3)}(x_{i})}{3!}h^{2} + \dots + \frac{f^{(n)}(x_{i})}{n!}h^{n-1} + \dots$$

$$f'(x_{i}) = \frac{-f(x_{i+2}) + 4f(x_{i+1}) - 3f(x_{i})}{2h} - \frac{h^{2}}{3}f'''(x) + \dots$$

$$f'(x_{i}) = \frac{-f(x_{i+2}) + 4f(x_{i+1}) - 3f(x_{i})}{2h} + O(h^{2})$$

	First Derivative	
Method	Formula	Truncation Error
Two-point forward difference	$f'(x_i) = \frac{f(x_{i+1}) - f(x_i)}{h}$	<i>0(h)</i>
Three-point forward difference	$f'(x_i) = \frac{-3f(x_i) + 4f(x_{i+1}) - f(x_{i+2})}{2h}$	$0(h^2)$
Two-point central difference	$f'(x_i) = \frac{f(x_{i+1}) - f(x_{i-1})}{2h}$	0(h)
Two-point backward difference	$f'(x_i) = \frac{f(x_i) - f(x_{i-1})}{h}$	0(<i>h</i> ²)
three-point central difference	$f'(x_i) = \frac{f(x_{i-2}) - 4f(x_{i-1}) + 3f(x_i)}{2h}$	$0(h^2)$
Four-point central difference	$f'(x_i) = \frac{f(x_{i-2}) - 8f(x_{i-1}) + 8f(x_{i+1}) - f(x_{i+2})}{12h}$	$0(h^4)$
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	Second Derivative	120
Method	Formula	Truncation Error
Three-point forward difference	$f''(x_i) = \frac{f(x_i) - 2f(x_{i+1}) + f(x_{i+2})}{h^2}$	0(h)
Four-point forward difference	$f''(x_i) = \frac{2 f(x_i) - 5 f(x_{i+1}) + 4 f(x_{i+2}) - f(x_{i+3})}{h^2}$	$0(h^2)$
Three-point backward difference	$f''(x_i) = \frac{f(x_{i-2}) - 2f(x_{i-1}) + f(x_i)}{h^2}$	0(h)
Four -point backward difference	$f''(x_i) = \frac{-3f(x_{i-3}) + 4f(x_{i-2}) - 5f(x_{i-1}) + 2f(x_i)}{h^2}$	$0(h^2)$
Three-point central difference	$f''(x_i) = \frac{f(x_{i-1}) - 2f(x_i) + f(x_{i+1})}{h^2}$	$0(h^2)$
Five-point central difference	$ \frac{f''(x_i) = \frac{-f(x_{i-2}) + 16 f(x_{i-1}) - 30 f(x_{i+1}) - 16 f(x_{i+1}) - f(x_{i+2})}{12h^2} $	$0(h^4)$

Finite Difference Methods for Solving PDE's



Numerical Analyses

1 Elliptic equation

The Laplace Equation $\frac{\partial^2 u}{\partial x^2} + \frac{\partial^2 u}{\partial y^2} = 0$

The Laplace molecule for $\Delta x = \Delta y = h$

$$u_{i+1,j} + u_{i-1,j} + u_{i,j+1} + u_{i,j-1} - 4 u_{i,j} = 0$$
$$u_{i,j} = \frac{1}{4} (u_{i+1,j} + u_{i-1,j} + u_{i,j+1} + u_{i,j-1})$$

This shows that the value of $u_{i,j}$ is the average of its values at the four neighboring diagonal mesh points. is called the **diagonal five-point formula** which is represented in Figure.

The temperature distribution can be estimated by discretizing the Laplace equation at 9 points and solving the system of linear equations.

$$u_{2,3} = \frac{1}{4}(b_{1,3}+u_{3,3}+u_{2,4}+u_{2,2})$$

$$u_{3,4} = \frac{1}{4}(u_{2,4}+u_{4,4}+b_{3,5}+u_{3,3})$$

$$u_{4,3} = \frac{1}{4}(u_{3,3}+b_{5,3}+u_{4,4}+u_{4,2})$$

$$u_{3,2} = \frac{1}{4}(u_{2,2}+u_{4,2}+u_{3,3}+u_{3,1})$$



Having found all the nine values of $u_{i,j}$ once, their accuracy is improved by either of the following iterative methods. In each case, the method is repeated until the difference between two consecutive iterates becomes negligible.

(*i*) **Jacobi's method.** Denoting the *n*th iterative value of $u_{i,j}$, by $u_{i,j}^n$, the iterative formula to solve is

$$u^{n+1}_{i,j} = \frac{1}{4} (u^n_{i+1,j} + u^n_{i-1,j} + u^n_{i,j+1} + u^n_{i,j-1})$$

It gives improved values of $u_{i,j}$ at the interior mesh points and is called the *point Jacobi's* formula.

(ii) Gauss-Seidal method. In this method, the iteration formula is

$$u^{n+1}_{i,j} = \frac{1}{4} \left(u^n_{i+1,j} + u^{n+1}_{i-1,j} + u^{n+1}_{i,j+1} + u^n_{i,j-1} \right)$$

It utilizes the latest iterative value available and scans the mesh points symmetrically from left to right along successive rows.

Example: A vertical steel plate of dimensions 2.7 cm X 2.7 cm and negligible thickness is in steady state conditions. On the top edge, the temperature is $100^{\circ}C$ and on the bottom the temperature is fixed at 50^o C. The temperature on the left and right edges are 50^o C. Solve to obtain heat distribution.



Numerical Analyses

Assistant Prof. Dr. Eng. Ibrahim Thamer Nazzal

Node or grid point (2,1),
$T_{11} + 50 - 4 T_{21} + T_{22} + 50 = 0$
or $T_{11} - 4T_{21} + T_{22} = -100$ (3)
Node or grid point (2,2),
$T_{12} + T_{21} - 4 T_{22} + 100 + 50 = 0$
$T_{12} + T_{21} - 4T_{22} = -150 \tag{4}$
From equations 1, 2, 3 and 4 we have
$-4T_{11} + T_{12} + T_{21} = -100 \tag{1}$
$T_{11} - 4T_{12} + T_{22} = -150 \tag{2}$
$T_{11} - 4T_{21} + T_{22} = -100\tag{3}$
$T_{12} + T_{21} - 4T_{22} = -150 \tag{4}$
$\begin{bmatrix} -4 & 1 & 1 & 0 \\ 1 & -4 & 0 & 1 \\ 1 & 0 & -4 & 1 \\ 0 & 1 & 1 & -4 \end{bmatrix} \begin{bmatrix} T_{11} \\ T_{12} \\ T_{21} \\ T_{22} \end{bmatrix} = \begin{bmatrix} -100 \\ -150 \\ -100 \\ -150 \end{bmatrix}$

solve this system of linear equations. Numerical Analyses **Example** Consider steady two-dimensional heat transfer in a long solid body whose cross section is given in the figure. The temperatures at the selected nodes and the thermal conditions on the boundaries are as shown. The thermal conductivity of the body is k 180 W/m \cdot °C, and heat is generated in the body uniformly at a rate of $g = 10^7 10 \text{W/m}_3$. Using the finite difference method with a mesh size of $\Delta x = \Delta y = 10$ cm, determine the temperatures at nodes 1, 2, 3, and 4 and 100 100 100 100°C Analysis: The nodal spacing is given to be $\Delta x = \Delta x = l = 0.1$ m, and the general finite difference form of an interior node $\dot{g} = 10^7 \, \text{W/m}^3$ equation for steady two-dimensional heat conduction for the (1)(2) case of constant heat generation is expressed as 120120 $u_{i,j} = \frac{1}{4} (u_{i+1,j} + u_{i-1,j} + u_{i,j+1} + u_{i,j-1})$ $T_{left} + T_{top} + T_{bottom} + T_{right} - 4 T_{node} + \frac{g_{node}}{r}$ There is summational (3) $(\mathbf{4})$ 150 150 0.1 m

There is symmetry about a vertical line passing through the middle of the region, and thus we need to consider only half of the region. Then,

200 200 200 200 $T_1 = T_2$ and $T_3 = T_4$ $\int V 100 + 120 + T_2 + T_3 - 4T_1 + \frac{gl^2}{k} = 0 \qquad \frac{\partial^2 T}{\partial x^2} + \frac{\partial^2 T}{\partial y^2} + \frac{\partial^2 T}{\partial z^2} + \frac{\dot{g}}{k} = \frac{1}{\alpha} \frac{\partial T}{\partial t}$ node 1 $150 + 200 + T_1 + T_4 - 4T_3 + \frac{gl^2}{l_2} = 0$ node 3 $T_1 = T_2$ and $T_3 = T_4$ and substituting noting that $200 + T_3 - 3T_1 + \frac{0.1^2 \times 10^7}{180} = 0$ The solution of the above system is $T_1 = T_2 = 411.5 \text{ C} \text{ and } T_3 = T_4 = 439 \text{ C}$ $350 + T_1 - 3T_3 + \frac{0.1^2 \times 10^7}{100} = 0$ 30 19.02.2025 Assistant Prof. Dr. Eng. Ibrahim Thamer Nazzal **Engineering Analysis**

0.1 m

Explicit and Implicit methods

Explicit and implicit methods are approaches used in <u>numerical analysis</u> for obtaining numerical approximations to the solutions of time-dependent <u>differential equations</u>.

Explicit Method = a formulation of equation into a FD equation that expresses **one** unknown in terms of the known values or express all future $(t + \Delta t)$ values, $T(x, t + \Delta t)$, in terms of current (t) and previous $(t - \Delta t)$ information, which is known.

Implicit methods calculate a solution by solving an equation involving both the current state of the system and the later one or **Implicit** Schemes express all future $(t + \Delta t)$ values, $T(x, t + \Delta t)$, in terms of other future $(t + \Delta t)$, current (t), and sometimes previous $(t - \Delta t)$ information.

Finite Difference Solution of Partial Differential Equations: Parabolic Equation



The explicit method

1. The explicit method - one unknown or nodal value is directly expressed in terms of known pivotal values. • *The process advancing from a known time level(s) to the unknown time level is called "time marching"*.

In this approaches using a forward difference at time *t* and a second order central difference for the space derivatives. $\partial u \quad \partial^2 u$

 $\frac{\partial u}{\partial t} = D \ \frac{\partial^2 u}{\partial x^2}$ Use a central difference approximation to evaluate $\frac{\partial^2 u}{\partial x^2}$ at *i*, *j* $\frac{\partial^2 u}{\partial x^2}\Big|_{i \ i} = \frac{u_{i+1,j} - 2 u_{i,j} + u_{i-1,j}}{(\Delta x)^2}$ *u*_{*i*.*i*+1} unknown values • Let's use a forward difference approximation to evaluate $\frac{\partial u}{\partial t}$ at *i*, *j* u _{i-1,j} $u_{i+1,j}$ и _{і,і} known values u = 0 $\frac{\partial u}{\partial t}\Big|_{i,i} = \frac{u(x_{i,j+1}) - u(x_{i,j})}{\Delta t}$ u = 0 Δt $u_{i,j-1}$ Δx Substituting into the main equation, one obtain $\frac{u_{i,j+1} - u_{i,j}}{\Delta t} = D \frac{u_{i+1,j} - 2 u_{i,j} + u_{i-1,j}}{(\Delta x)^2}$ $u_{i,j+1} = u_{i,j} + \Delta t D \frac{u_{i+1,j} - 2 u_{i,j} + u_{i-1,j}}{(\Delta x)^2}$ x_m u = f(x)Define the parameter *r* as $r = \frac{D \Delta t}{(\Delta x)^2}$

Assistant Prof. Dr. Eng. Ibrahim Thamer Nazzal

19.02.2025

$$(u_{i,j+1} - u_{i,j}) = r (u_{i+1,j} - 2 u_{i,j} + u_{i-1,j})$$

$$u_{i,j+1} = r u_{i+1,j} + [1 - 2r] u_{i,j} + r u_{i-1,j}$$
We can write out the matrix system of equations we will solve numerically for the temperature u .
Finite difference method PDE example (heat equation)

$$u_{i,j+1} = r u_{i+1,j} + [1 - 2r] u_{i,j} + r u_{i-1,j} \quad \text{can be written as}$$

$$u_{j+1} = A u_{j}$$

$$A = \begin{bmatrix} 1 - 2r & r & & \\ r & 1 - 2r & r & \\ & \ddots & \ddots & & \\ & & \ddots & \ddots & r & \\ & & & r & 1 - 2r \end{bmatrix}, \quad U \triangleq \begin{bmatrix} u_{0} \\ u_{1} \\ \vdots \\ \vdots \\ u_{J} \end{bmatrix}.$$
Associated with the provement of the temperature of tem

contact with blocks of melting ice and that the initial temperature distribution in nondimensional form (unitless) is

i) u = 0 at x = 0 and x = 1, t > 0 (the boundary condition) 0 < x < 1ii) u = 2x, for $0 \le x \le \frac{1}{2}$ u = 2(1-x), for $\frac{1}{2} \le x \le 1$ t = 0 (the initial condition) $\frac{\partial u}{\partial t} = \frac{\partial^2 u}{\partial x^2}$ using the Explicit Method

 $r = \frac{\Delta t}{(\Delta x)^2} = \frac{1}{10} \qquad y$

Solve the heat conduction equation

$$\Delta x = h = 0.1 \quad \Delta t = 0.001$$

solution

$$u_{0,0} = 0, u_{1,0} = 0.2, u_{3,0} = 0.6, u_{2,0} = 0.4 u_{4,0} = 0.8, u_{5,0} = 1, u_{i,j} = 1, u_{i,j} = 1, u_{i+1,j} = 1, u_{$$

Numerical Analyses

Assistant Prof. Dr. Eng. Ibrahim Thamer Nazzal

	i=0	i=1	i=2	i=3	i=4	i=5	i=6
	x=0	0,1	0,2	0,3	0,4	0,5	0,6
(i=0)t=0,000	0	0,2000	0,4000	0,6000	0,8000	1,000	0,8000
(i=1)= 0,001	0	0,2000	0,4000	0,6000	0,8000	0,9600	0,8000
(i=2)= 0,002	0	0,2000	0,4000	0,6000	0,7960	0,9280	0,7960
(i=3)= 0,003	0	0,2000	0,4000	0,5996	0,7896	0,9016	0,7896
(i=4)= 0,004	0	0,2000	0,4000	0,5986	0,7818	0,8792	0,7818
(i=5)= 0,005	0	0,2000	0,3999	0,5971	0,7732	0,8597	0,7732
(i=10)= 0,01	0	0,1996	0,3968	0,5822	0,7281	0,7867	0,7281
(i=20)= 0,02	0	0,1938	0,3781	0,5373	0,6486	0,6891	0,6486

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Numerical Analyses

5

Assistant Prof. Dr. Eng. Ibrahim Thamer Nazzal

Example: Consider a steel rod that is subjected to a temperature of 100 C on the left end and 25 C on the right end. If the rod is of length 0.05 m, use the explicit method to find the temperature distribution in the rod from t = 0 and t = 9 seconds. Use $\Delta x = 0.01$ and $\Delta t = 3 s$ Given: $k = 54 \frac{W}{m^2 K} \rho = 7800 \frac{kg}{m^3}, C = 490 \frac{j}{kg,K}$ The initial temperature of the rod is 20 C. i = 01 3 2 **Solution** $T = 25^{\circ}$ $T = 100 \circ C$ 0.01mNumber of time steps, Recall, $\frac{t_{final} - t_{initial}}{\Delta t}$ $= \frac{9 - 0}{2} = 3$ $\alpha = \frac{\kappa}{\rho C}$ therefore, $\alpha = \frac{51}{7800 \times 490}$ **Boundary Conditions** $\begin{array}{c} T_0^{\ j} = 100^{\circ}C \\ T_5^{\ j} = 25^{\circ}C \end{array} \right\} \quad \text{for all } j = 0,1,2,3$ $= 1.4129 \times 10^{-5} m^2$ Then, All internal nodes are at $= 1.4129 \times 10^{-5} \frac{3}{(0.01)^2} = 0.4239$ for t = 0 sec This can be represented as, $T_i^0 = 20^{\circ}C$, for all i = 1, 2, 3, 436

Nodal temperatures when $t = 0 \sec j$, j = 0:

 $T_0^0 = 100^{\circ}C$ $T_1^0 = 20^{\circ}C$ $T_2^0 = 20^{\circ}C$ { Interior nodes $T_{3}^{0} = 20^{\circ}C$ $T_{4}^{0} = 20^{\circ}C$ $T_{5}^{0} = 25^{\circ}C$

merNazza We can now calculate the temperature at each node explicitly using the equation formulated

earlier, $T_{i}^{j+1} = T_{i}^{j} + \lambda (T_{i+1}^{j} - 2T_{i}^{j} + T_{i-1}^{j})$ rahim Nodal temperatures when $t = 3 \sec t$ i = 0 $T_0^1 = 100^\circ C - Boundary Condition$ setting j=0 $\underline{i=1} \quad T_1^1 = T_1^0 + \lambda \left(T_2^0 - 2T_1^0 + T_0^0 \right) \\ = 20 + 0.4239 (20 - 2(20) + 100) \quad \underline{i=2} \quad T_2^1 = T_2^0 + \lambda \left(T_3^0 - 2T_2^0 + T_1^0 \right) \\ = 20 + 0.4239 (20 - 2(20) + 100) \quad \underline{i=2} \quad T_2^1 = T_2^0 + \lambda \left(T_3^0 - 2T_2^0 + T_1^0 \right) \\ = 20 + 0.4239 (20 - 2(20) + 100) \quad \underline{i=2} \quad T_2^1 = T_2^0 + \lambda \left(T_3^0 - 2T_2^0 + T_1^0 \right) \\ = 20 + 0.4239 (20 - 2(20) + 100) \quad \underline{i=2} \quad T_2^1 = T_2^0 + \lambda \left(T_3^0 - 2T_2^0 + T_1^0 \right) \\ = 20 + 0.4239 (20 - 2(20) + 100) \quad \underline{i=2} \quad T_2^1 = T_2^0 + \lambda \left(T_3^0 - 2T_2^0 + T_1^0 \right) \\ = 20 + 0.4239 (20 - 2(20) + 100) \quad \underline{i=2} \quad T_2^1 = T_2^0 + \lambda \left(T_3^0 - 2T_2^0 + T_1^0 \right) \\ = 20 + 0.4239 (20 - 2(20) + 100) \quad \underline{i=2} \quad T_2^1 = T_2^0 + \lambda \left(T_3^0 - 2T_2^0 + T_1^0 \right) \\ = 20 + 0.4239 (20 - 2(20) + 100) \quad \underline{i=2} \quad T_2^0 + 0.4239 (20 - 2(20) + 100) \quad \underline{i=2} \quad T_2^0 + 0.4239 (20 - 2(20) + 100) \quad \underline{i=2} \quad T_2^0 + 0.4239 (20 - 2(20) + 100) \quad \underline{i=2} \quad T_2^0 + 0.4239 (20 - 2(20) + 100) \quad \underline{i=2} \quad T_2^0 + 0.4239 (20 - 2(20) + 100) \quad \underline{i=2} \quad T_2^0 + 0.4239 (20 - 2(20) + 100) \quad \underline{i=2} \quad T_2^0 + 0.4239 (20 - 2(20) + 100) \quad \underline{i=2} \quad \underline{i=2} \quad T_2^0 + 0.4239 (20 - 2(20) + 100) \quad \underline{i=2} \quad \underline{i=$ = 20 + 0.4239(20 - 2(20) + 20)= 20 + 0.4239(80)= 20 + 0.4239(0)= 20 + 33.912= 20 + 0 $= 53.912^{\circ}C$ $= 20^{\circ}C$ Nodal temperatures when $t = 3 \sec i$, j = 1: $T_0^1 = 100^{\circ}C$ – Boundary Condition $T_1^1 = 53.912^{\circ}C$ $T_{2}^{1} = 20^{\circ}C$ **Interior nodes** $T_{3}^{1} = 20^{\circ}C$ $T_5^1 = 25^{\circ}C$ – Boundary Condition $T_4^1 = 22.120^{\circ}C$ Assistant Prof. Dr. Eng. Ibrahim Thamer Nazzal Numerical Analyses

Nodal temperatures when $t = 6 \sec t$ $T_0^2 = 100^{\circ}C - Boundary Condition$ setting j=1, $\underbrace{i=2}_{0} T_2^2 = T_2^1 + \lambda (T_3^1 - 2T_2^1 + T_1^1)$ = 20 + 0.4239(20 - 2(20) + 53.912) = 20 + 0.4239(33.912) i = 1 $T_1^2 = T_1^1 + \lambda (T_2^1 - 2T_1^1 + T_0^1)$ = 53.912 + 0.4239 (20 - 2(53.912) + 100)= 20 + 0.4239(33.912)= 53.912 + 0.4239(12.176)= 20 + 14.375= 53.912 + 5.1614 $=34.375^{\circ}C$ $= 59.073^{\circ}C$ Nodal temperatures when $t = 6 \sec j = 2$: $T_0^2 = 100^{\circ}C$ – Boundary Condition $T_1^2 = 59.073^{\circ}C$ $T_{2}^{2} = 34.375^{\circ}C$ $T_{3}^{2} = 20.889^{\circ}C$ $T_{4}^{2} = 22.442^{\circ}C$ Interior nodes $T_{5}^{2} = 25^{\circ}C - \text{Boundary Condition}$ Nodal temperatures when $t = 9 \sec t$ i=0 $T_0^3 = 100^{\circ}C - Boundary Condition$ setting j = 2, \checkmark i = 2i = 1 $T_1^3 = T_1^2 + \lambda (T_2^2 - 2T_1^2 + T_0^2)$ $T_2^3 = T_2^2 + \lambda (T_3^2 - 2T_2^2 + T_1^2)$ = 34.375 + 0.4239(20.899 - 2(34.375) + 59.073)=59.073+0.4239(34.375-2(59.073)+100)**S**=59.073+0.4239(16.229) = 34.375 + 0.4239(11.222)= 59.073 + 6.8795= 34.375 + 4.7570 $= 39.132^{\circ}C$ $= 65.953^{\circ}C$

Nodal temperatures when $t = 9 \sec$,

 $T_{0}^{3} = 100^{\circ}C - \text{Boundary Condition}$ $T_{1}^{3} = 65.953^{\circ}C$ $T_{2}^{3} = 39.132^{\circ}C$ $T_{3}^{3} = 27.266^{\circ}C$ $T_{4}^{3} = 22.872^{\circ}C$ $T_{5}^{3} = 25^{\circ}C - \text{Boundary Condition}$

To better visualize the temperature variation at different locations at different times, the temperature distribution along the length of the rod at different times is plotted below.

j = 3



Numerical Analyses

39

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